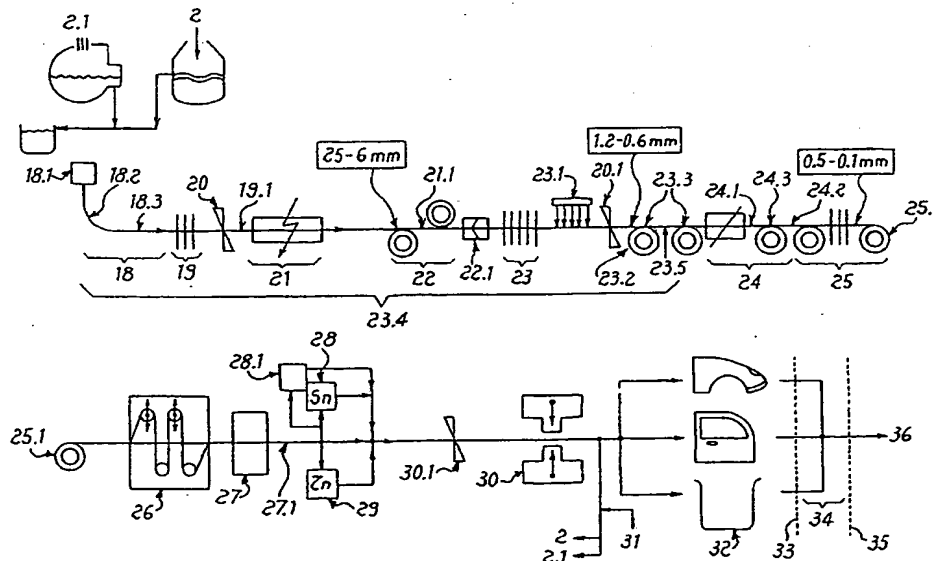




INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(51) International Patent Classification ⁶: B21B 1/46, 1/00	A1	(11) International Publication Number: WO 00/20141 (43) International Publication Date: 13 April 2000 (13.04.00)
(21) International Application Number: PCT/IT99/00018 (22) International Filing Date: 27 January 1999 (27.01.99) (30) Priority Data: MI98A002116 1 October 1998 (01.10.98) IT (71)(72) Applicant and Inventor: ARVEDI, Giovanni [IT/IT]; Via Mercatello, 26, I-26100 Cremona (IT). (74) Agents: ADORNO, Silvano; Società Italiana Brevetti S.p.A., Via Carducci, 8, I-20123 Milano (IT) et al.		(81) Designated States: AL, AM, AT, AU, AZ, BA, BB, BG, BR, BY, CA, CH, CN, CU, CZ, DE, DK, EE, ES, FI, GB, GE, GH, GM, HR, HU, ID, IL, IN, IS, JP, KE, KG, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MD, MG, MK, MN, MW, MX, NO, NZ, PL, PT, RO, RU, SD, SE, SG, SI, SK, SL, TJ, TM, TR, TT, UA, UG, US, UZ, VN, YU, ZW, ARIPO patent (GH, GM, KE, LS, MW, SD, SZ, UG, ZW), Eurasian patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European patent (AT, BE, CH, CY, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, GW, ML, MR, NE, SN, TD, TG). Published <i>With international search report.</i>

(54) Title: PROCESS AND RELATIVE PRODUCTION LINE FOR THE DIRECT MANUFACTURE OF FINISHED PRESSED OR DEEP DRAWN PIECES FROM ULTRATHIN HOT ROLLED STRIP CAST AND ROLLED IN-LINE

**(57) Abstract**

A process for the production of cold rolled finished strip with thickness of 0.5-0.1 mm and a maximum width of 2000 mm for direct preparation of end products such as pressed and deep drawn pieces from thin slab casting with a thickness of the bar leaving the mould of 90-50 mm, with preparation of pressed pieces and transfer of the finished pieces to the end user and return of the processing scrap to the steel manufacturing cycle. Also a production line for carrying out such a process is described.

FOR THE PURPOSES OF INFORMATION ONLY

Codes used to identify States party to the PCT on the front pages of pamphlets publishing international applications under the PCT.

AL	Albania	ES	Spain	LS	Lesotho	SI	Slovenia
AM	Armenia	FI	Finland	LT	Lithuania	SK	Slovakia
AT	Austria	FR	France	LU	Luxembourg	SN	Senegal
AU	Australia	GA	Gabon	LV	Latvia	SZ	Swaziland
AZ	Azerbaijan	GB	United Kingdom	MC	Monaco	TD	Chad
BA	Bosnia and Herzegovina	GE	Georgia	MD	Republic of Moldova	TG	Togo
BB	Barbados	GH	Ghana	MG	Madagascar	TJ	Tajikistan
BE	Belgium	GN	Guinea	MK	The former Yugoslav Republic of Macedonia	TM	Turkmenistan
BF	Burkina Faso	GR	Greece	ML	Mali	TR	Turkey
BG	Bulgaria	HU	Hungary	MN	Mongolia	TT	Trinidad and Tobago
BJ	Benin	IE	Ireland	MR	Mauritania	UA	Ukraine
BR	Brazil	IL	Israel	MW	Malawi	UG	Uganda
BY	Belarus	IS	Iceland	MX	Mexico	US	United States of America
CA	Canada	IT	Italy	NE	Niger	UZ	Uzbekistan
CF	Central African Republic	JP	Japan	NL	Netherlands	VN	Viet Nam
CG	Congo	KE	Kenya	NO	Norway	YU	Yugoslavia
CH	Switzerland	KG	Kyrgyzstan	NZ	New Zealand	ZW	Zimbabwe
CI	Côte d'Ivoire	KP	Democratic People's Republic of Korea	PL	Poland		
CM	Cameroon	KR	Republic of Korea	PT	Portugal		
CN	China	KZ	Kazakstan	RO	Romania		
CU	Cuba	LC	Saint Lucia	RU	Russian Federation		
CZ	Czech Republic	LI	Liechtenstein	SD	Sudan		
DE	Germany	LK	Sri Lanka	SE	Sweden		
DK	Denmark	LR	Liberia	SG	Singapore		
EE	Estonia						

"PROCESS AND RELATIVE PRODUCTION LINE FOR THE DIRECT
MANUFACTURE OF FINISHED PRESSED OR DEEP DRAWN PIECES FROM
ULTRATHIN HOT ROLLED STRIP CAST AND ROLLED IN-LINE"

5 The present invention concerns a process and relative production line for the direct manufacture of finished pressed or deep drawn pieces from ultrathin hot strip cast and rolled in-line.

Worldwide production of hot rolled strip for the manufacture of cold rolled strip amounts to about 40% of world steel production which is currently about 750 million
10 tonnes/year. This share of cold rolled steel production in industrial countries amounts to about 50%, however, from which it can be deduced that the growth potential for hot or cold rolled strip production is very high at a worldwide level.

At the same time it must be remembered that the investment costs for traditional production lines are very high and, on the basis of an integral cycle steel mill with a
15 capacity of about 4 million tonnes/year, expressed in specific investment costs, amount to about US\$ 1000/tonne of cold rolled strip.

A traditional process and production line for the manufacture of cold rolled strip with gauges from 0.6 to 0.1 mm, coated or non-coated, is composed for example, as shown in figure 1 relative to the prior art, of:

- 20 - blast furnace production (1);
- oxygen melt shop (2) - convertor;
- continuous slab casting plant with thickness 200-250 mm and width 800-2600 mm (3);
- hot rolling mill (4) composed of a furnace (4.1), a roughing mill (4.2) and a
25 finishing mill (4.3) for the manufacture of hot strip in gauges between 4 and 2 mm and a maximum width of 1800 mm for the manufacture of cold rolled strip;
- continuous pickling (5);
- cold rolling mill (6), for example as a continuous or reversible rolling mill for
30 the manufacture of gauges between 0.6 and 0.3 mm;
- annealing (7) of the continuous or bell type;
- cold finishing mill (skinpass mill) with temperature management and control (8).

This cold rolled strip, controlled as regards thickness, crown and flatness, will
35 feed at choice: a tinning line (9) or a galvanizing line (10) or, without surface coating, a service centre directly (11) where, depending on customer requirements, it will be

transformed in the form of strip or packs of sheet, depending on the orders, to then leave the factory (12) by transport on road, rail and/or water (13). This traditional form of selling finished cold rolled strip also involves the transport of the processing scrap (16) produced by those who carry out subsequent processing (14). This scrap
5 derives, for example, from pressing or deep drawing (15) of finished parts such as, for example, assembly components (boxes, car and tank pieces etc.). This processing scrap (16), which currently amounts to about 15% of the whole of worldwide steel production, can be seen as a "steel tare" which is transported uselessly from the steel manufacturer (12) to the customer (14) to return once more to the steel manufacturer
10 (12) and consequently implies transport costs in the form of time, energy and environmental pollution.

The customer (14) traditionally collects from the steel mill sheets or coils which are suitable for deep drawing and pressing, preferably with a carbon content below 0.06%. The customer unwinds them and puts them for example into a press (15) in
15 order to obtain products (17) such as:

- press-processed pieces or
- deep drawn pieces such as, for example, external or internal parts for the construction of cars or lorries.

The scrap derived from processing (16), also defined as "new scrap", produced
20 from the pressing of sheets at the customer's or end user's (14) and as a share of tare already amounts to about 30% of total scrap production, which currently corresponds to about 50% of world steel production, must be transported back to steel manufacturing, such as an oxygen melt shop (2) or an electric mill (2.1), causing consequent costs. This means that the scrap makes its way again to the steel
25 manufacturer's to be recycled.

Moreover, this production line is characterized by a longitudinal dimension of about 1500-2000 metres and a transversal dimension of about 50 metres, calculated from the continuous casting plant (3) to shipment (11) of the cold rolled product in the form of coils (11.1) or packs of sheet (11.2). Moreover, each manufacturing phase is
30 generally equipped with an uncoiling and coiling station which in addition causes expenditure of work, loss of energy and material, as well as possible operating anomalies, and also requires space for storage and moving the coils between one production phase and the subsequent one.

An initial shortening of the casting and rolling processes, and therefore a cost
35 reduction in the price per tonne of hot rolled strip of about 50%, could be achieved with the introduction of the thin slab technique together with the continuous finishing mill. As regards this, the so-called ISP (In-line Strip Production) process in particular,

with the components of the cast-rolling technique, i.e. slab thickness reduction during and immediately after the solidification phase, is to be cited (DE 38 40 812, DE 38 18 077, DE 44 03 048 and DE 44 03 049). This technology, compared with other thin slab technologies which show no thickness reduction, leads to a reduction of up to 50% during the solidification phase and up to 80% directly after solidification, a better surface quality and, at the same time, a finer crystalline structure, improved internal quality and, therefore, considerably improved properties of the material in the end product.

In the ISP process (23.4) for example, which is represented in part of figure 2, the slab casting thickness (18.3) in the thin slab casting plant (18) is reduced during solidification in the roll table (18.2) from a thickness of 65 mm on leaving the mould (18.1) to a minimum thickness of 30 mm. Directly after solidification the slab thickness is reduced to as low as 6 mm by means of a rolling process, for example through three small stands (19) with an entry speed from 0.666 to a maximum of 0.15 m/s.

These cast-rolling technologies during and directly after solidification produce slabs with very good surface characteristics and a central-symmetrical and controlled convexity (crown) for example of 1.0-1.5% on a thickness of 6-25 mm, good flatness as well as a uniform grain size structure with minimum degrees of slab deformation from 30 mm to a minimum thickness of 6 mm or with a lengthening of 5 times.

The good production of the thin slab (18.3) and above all of the intermediate strip (19.1) in its shape and structure is to be traced back to the rolling in casting during solidification and above all to the rolling process after solidification which is characterized by a considerable transversal flow of the thin slab to be rolled in the pass between the rolls. This transversal flow is caused by the low deformation speed and the low resistance to rolling in the transversal direction of the material from thin slabs. Moreover, the good behaviour of the flow of the rolling material (18.3) in the pass between the roughing mill rolls (19) is directly favoured, after solidification, by the low deformation force at the high average temperature of 1350°C in the cross-section of the slab. Moreover, the slab (18.3) with a surface temperature of about 1200°C on entry to the first rolling stand of the roughing mill (19) still has a thermal gradient, i.e. a temperature increase in the direction of the slab nucleus.

This external and internal temperature between the solidification point and entry to the first stand is controllable by cooling and favours a current of the uniform mass on the cross-section of the slab in the pass between the rolling cylinders: i.e. it allows a uniform degree of deformation on the slab thickness or better on the thickness of the material to be rolled. This intermediate product (19.1), cast and rolled during and

directly after solidification, presents the following characteristics:

- thickness of 6-25 mm;
- width of 700-2000 mm;
- central symmetrical crown between 1.0 and 1.5%;
- 5 - central symmetry of the convexity $> 95\%$ (wedge) on the width of the material to be rolled;
- high degree of flatness of the material to be rolled;
- better surface quality, which meets the high demands for the deep drawing (05/05) of external automobile parts;
- 10 - uniform, homogeneous and transversally fine crystalline structure which leads to high resistance and toughness as well as excellent ductility for good cold deformation;

This intermediate rolled product (19.1) manufactured in this way with its positive characteristics, which a rolled product produced according to the prior art does not usually show, with a thickness of 25-6 mm derived from the traditional slab between points (3) and (4.6) having a thickness of 280-150 mm, or from a conventional thin slab with a thickness of 50 mm, is now heated, preferably by means of an induction furnace (21), to an optimal temperature in relation to the form of rolling which is determined by:

- 20 - the steel grade;
- the final rolling thickness;
- management of the hot strip temperature in the rolling mill (23) between the first and the n-th stand as also in the cooling line (23.1) and in the hot rolled strip coiler (23.2);
- 25 - recrystallization and formation of the structure with respect to the material and its behaviour in the T.T.T. diagram (time-temperature-transformation);
- crown;
- flatness

30 to be then taken directly or again coiled into an intermediate coil (22) at the rolling mill (23) for example by means of a form of continuous rolling without longitudinal cutting of the slab (18.3). In the rolling mill (23) the hot strip (23.3) with a thickness between 1.2 and 0.6 mm finally reaches the hot strip coiler (23.2) for recrystallization, from where it is then taken to other processing processes at the cold rolling mill (25) with or without subsequent surface coating.

35 The task of the invention is now that of considerably simplifying the traditional hot rolled strip production process described above and based on the traditional slab or

even on a normal thin slab (figure 1) with the help of the ISP process (23.4) and a rolling product with a thickness of 0.6-1.2 mm, saving stages in the process, reducing costs and having the possibility of directly preparing, subsequently to the rolling process, for example finished pressed or deep drawn pieces such as details for a car door, pieces which are then supplied as finished products (32) to the end user i.e. the car manufacturer for final assembly.

This technology would lead to savings in the following sectors:

- investment costs;
- manufacturing costs:
- 10 • energy
- material
- salaries and wages
- transport
- cost per piece
- 15 as well as improvements as regards environmental pollution, supported by:
- savings in the annealing process;
- savings in transport energy and
- better exploitation of the material (recycling).

The ISP process (23.4), together with processes according to the present invention which include the further processing of the material, leads to an innovative solution of the problem, characterized by the claims of the process and the production lines.

The present invention will now be described in greater detail with reference to an example of embodiment on the basis of the attached drawings in which:

25 FIGURE 1 shows a traditional process method and relative production line for the manufacture of cold rolled products and finished products derived therefrom, as already exhaustively described, which describes the present state of the art; and

FIGURE 2 shows an inventive combination of the process and the production line for the manufacture of cold rolled finished products based on the casting of thin slabs with the cast-rolling technique during and after solidification.

30 The tests conducted on an ISP plant which represent the bases of the process and the production lines according to the invention are described with the aid of Fig. 2.

 The newly invented process and production line presuppose the melting of the steel in a BOF oxygen (converter) (2) or electric (2.1) melt shop and are based on a thin slab plant (18) with a thickness on leaving the mould (18.1) for example between 50 and 90 mm and for example with a thickness reduction during solidification to 30 mm minimum. A small roughing mill (19) is connected to the continuous casting plant

directly in-line and passes the thin slab (18.3) with a casting speed of about 4-8 m/min thus producing a high transversal flow of the rolling material (18.3) in the passage between the rolling cylinders. By means of this transversal flow and, not least, by means of the controlled thermal gradient between the slab surface and the slab nucleus, a very good and symmetrical crown is obtained on the roughed strip (19.1) equal to 1.0-1.5% as well as a fine and uniform structure of the material on the strip cross-section.

The intermediate strip (19.1) at the end of the roughing mill (19) has a thickness of 25-6 mm and can be cut with the shear (20) into coils with a specific weight of 15-25 kg/mm width. After the roughing mill the intermediate strip (19.1) preferably flows into an induction furnace (21) by means of which it is brought to an optimal temperature for the end product depending on the steel grade, the strip thickness and the desired structure of the material or rather the desired properties of the material. Following the temperature control the strip with rolled structure rolls into an intermediate coiler (22) where the specific temperature of the coil can be balanced again during the time the strip stays in the coiler.

It is also possible to achieve continuous rolling (21.1) in such a way that the strip (19.1), without coiling into an intermediate coil, is taken directly to the descaler (22.1) and the finishing mill (23). The intermediate strip (19.1) leaves the continuous roller table (23) as a hot strip (23.3) with a thickness of 1.2-0.6 mm and a width of 700-2000 mm, passes through the cooling area (23.1) with the aim of controlling the structure according to the T.T.T. diagram and passes through a shear (20.1) to be then wound into a hot coil (23.2). This hot strip (23.3) is taken to and maintained at a controlled temperature along the whole rolling line between the induction furnace (21) and the coiler for hot strip (23.2) in such a way as to maintain a controlled recrystallized and uniform structure as per the T.T.T. diagram. This hot strip (23.2), with its structure (23.3) controlled, can then, after pickling (24) be sent directly (24.2) or through intermediate coiling (24.3) to the cold rolling mill (25).

Moreover, the hot strip (23.3) can also be sent directly (23.5) to pickling without being wound on the coiler for hot strip (23.2).

In the cold rolling mill (25) the hot strip is cold rolled down to a thickness of 0.5-0.1 mm. After the cold rolling stage the strip (25.1) is taken to a cold finishing mill (27) with temperature management (26). After passing through the cold finishing mill (skinpass mill) (27) the strip is controlled as regards:

- thickness
- crown
- flatness

- structure

and taken directly to a surface coating line such as, for example, a tinning line (28), a galvanizing line (29), an organic coating line (28.1) or without a coating directly to a press (30). Here the finished products (32) are prepared directly at the steel manufacturer's, or rather at the cold rolled steel manufacturer's, products such as:

- pressed elements
- deep drawn elements

and the processing scrap (31) produced in the pressing process can be sent directly and therefore recycled at the steel melting process (2) or (2.1) with savings in transport costs and transport energy.

Leaving the steel manufacturer's factory door (33) are finished products, net-finished pieces (32) without "steel tare" (31) which can be taken directly to the customer's (35) for final assembly (36).

If the traditional production method is compared with the new inventive solution, it can be seen that through production of very thin, recrystallized, hot rolled strip (23.3) in gauges between 1.2 and 0.6 mm, for example with ISP technology (23.4), very thin strips (25.1) can be produced in the cold rolling mill (25) in gauges 0.5-0.1 mm. This thin cold strip (25.1) is processed directly in the cold finishing mill (27) with temperature management (26) in order to obtain the finished product (27.1) without having to use a traditional continuous annealing furnace with long control times of the material temperature.

The ready cold strip manufactured in this way (27.1) can then at choice be introduced into surface coating lines (28), (28.1) and (29) and/or fed directly to the press (30) for the production of finished pieces (32). This preparation phase (30), directly connected to the cold rolling mill (25) and the cold finishing mill (27) for the production of finished pieces (32), again leads to a reduction in energy, transport costs and environmental pollution.

The technical process invention with its relative production lines, compared with the traditional preparation line based on the traditional slab or the thin slab without thickness reduction during and after solidification, leads to a very thin hot strip (23.3), precise in its geometrical and recrystallized form, with a thickness between 1.2 and 0.6 mm and a crown between 1.0 and 1.5% or 10-15 microns which, after pickling, allows production of a finished cold rolled and ready strip (27.1) without traditional annealing. This ready cold strip rolled in this way, which implies low costs, is taken coated or not coated, directly to the press (30) for the production of the finished products (32) where, with the recycling of the processing scrap (31) in the melt shop nearby, further costs are saved.

The savings and/or advantages of the inventive new process with its relative production lines are:

- annealing, bell or continuous annealing, after cold rolling;
 - transport costs for the processing scrap due to production of the finished product
5 (32) at the steel manufacturer's instead of the end user's (35), as usual up to now;
and
 - savings in the following fields:
 - investment costs
 - manufacturing costs
10
 - energy
 - material
 - salaries and wages
 - transport
- cost per piece.

CLAIMS

1. A process for the manufacture of cold rolled and finished strip in gauges 0.5-0.1 mm and a maximum width of 2000 mm for the direct preparation of end products such as pressed and deep drawn pieces, which includes the following steps:

- casting for thin slabs with a thickness of the bar leaving the mould of 90-50 mm;
- bar thickness reduction during solidification to a minimum of 30 mm;
- slab thickness reduction directly after solidification connected to the casting process to a minimum of 6 mm (roughing stage);
- temperature regulation and control of the cast-rolled slab directly after the roughing phase;
- production of a cast-rolled product controlled as regards temperature, thickness, width, crown and flatness;
- finishing rolling in order to obtain a recrystallized hot coil with a thickness of 1.2 - 0.6 mm and a crown of 1.0-1.5%;
- pickling process with subsequent cold rolling for the production of cold strip of a thickness between 0.5 and 0.1 mm;
- cold finishing (skinpass) preceded by temperature management for the control of the structure of the material;
- preparation of pressed pieces with the return of the processing scrap to the steel manufacturing cycle;
- sending of finished pieces to the end user.

2. A process according to claim 1, characterized in that the intermediate strip is hot rolled directly in the finishing mill without winding into an intermediate coil (21.1).

3. A process according to claims 1 and 2, characterized in that the hot strip is sent directly to pickling without winding into an intermediate coil.

4. A process according to claims 1 to 3, characterized in that the pickled hot rolled strip is rolled in the cold rolling mill without winding into an intermediate coil.

5. A process according to claims 1 to 4, characterized in that between the cold finishing and pressing steps a coating of the cold rolled strip can be inserted.

6. A production line for carrying out the process according to one of the above-mentioned claims, including:

- a thin slab plant (18) with a hydraulically operated oscillating mould (18.1) and a thickness on leaving the mould of between 90 and 50 mm, a maximum width of 2000 mm and a maximum casting speed of 10 m/min;
- a roller table (18.2) composed exclusively of rolls which allows a thickness reduction of the slab (18.3) during solidification to a minimum of 30 mm;
- a roughing mill (19) composed of at least one stand, connected directly and in-line with

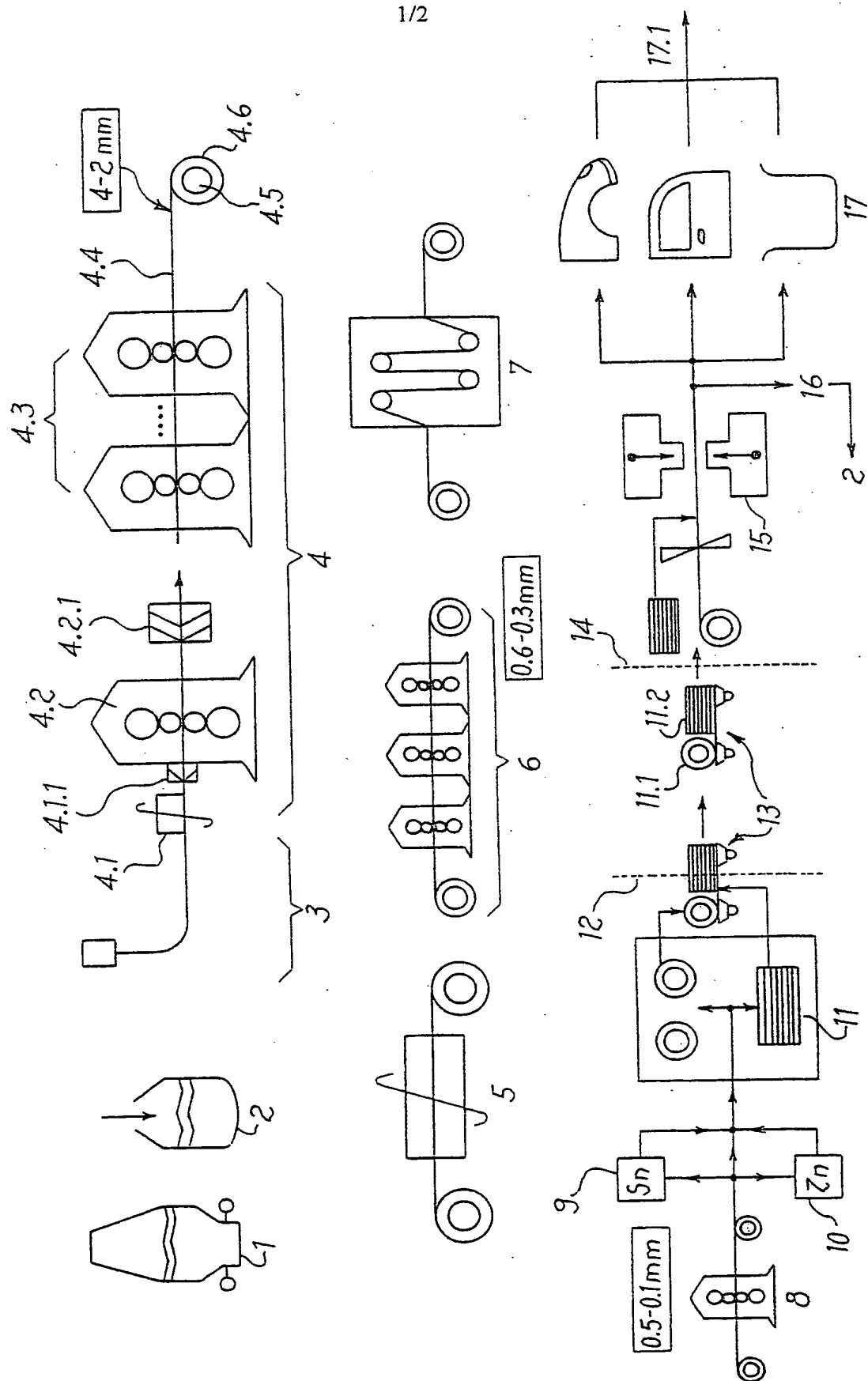
- the continuous casting plant (18) for the reduction or roughing of the slab (18.3) to a thickness of the roughed strip (19.1) from 25 mm to a minimum of 6 mm;
- a furnace, preferably induction furnace (21), for temperature control of the intermediate strip (19.1) directly after the roughing mill (19);
 - a finishing mill (23) which includes at least four stands, a cooling table (23.1) and a coiler for hot strip (23.2);
 - a pickling unit (24) with a cold rolling mill attached (25) for the manufacture of cold rolled strips in gauges 0.5-0.1 mm;
 - a finishing mill (27) with temperature control (26);
 - a press (30) for the manufacture of finished products (32) with return of the processing scrap (31) to the melt shop (2) or (2.1);
 - shipment of the finished product from the steel manufacturer's factory (33) to the end customer (35).

7. A production line according to claim 6, characterized in that between the roughing mill (19) and the finishing mill (23) the intermediate strip (19.1) is hot rolled (23.3) directly (21.1) in the finishing mill (23) and passes through a shear (20.1) before the downcoiler (23.3) without using or foreseeing the intermediate coiler (22).

8. A production line according to claims 6 and 7, characterized in that the hot strip (23.3) is sent directly (23.5) to pickling (24) without being wound in the coiler for hot strip (23.2).

9. A production line according to claims from 6 to 8, characterized in that the hot pickled strip (24.1) is rolled directly (24.2) into cold strip (25.1) in the cold rolling mill (25) without being wound into an intermediate coil (24.3).

10. A production line according to claims from 6 to 9, characterized in that between the cold finishing mill (27) and the press (30) a strip coating plant (28), (28.1) or (29) is foreseen.

Fig. 1

INTERNATIONAL SEARCH REPORT

Int. Patent Application No

PCT/IT 99/00018

A. CLASSIFICATION OF SUBJECT MATTER
IPC 6 B21B1/46 B21B1/00

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 6 B21B B21D

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	WO 98 00248 A (HOOGOVS STAAL BV) 8 January 1998	1,6
A	see page 19, line 6 - line 10; figures see page 20, line 21 - page 21, line 1 see page 21, line 18 - page 23, line 8 see page 27, line 23 - page 30, line 18 ---	3,5,8,10
A	EP 0 605 947 A (KAISER ALUMINIUM CHEM CORP) 13 July 1994 see page 2, line 3 - line 4 see page 3, line 7 - line 10 see page 2, line 24 - line 30 see page 3, line 31 - line 39 see page 6, line 42 - line 46 --- -/--	1,6

☒ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

* Special categories of cited documents :

- "A" document defining the general state of the art which is not considered to be of particular relevance
- "E" earlier document but published on or after the international filing date
- "L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)
- "O" document referring to an oral disclosure, use, exhibition or other means
- "P" document published prior to the international filing date but later than the priority date claimed

- "T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
- "X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
- "Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.
- "&" document member of the same patent family

Date of the actual completion of the international search

23 April 1999

Date of mailing of the international search report

29/04/1999

Name and mailing address of the ISA
European Patent Office, P.B. 5818 Patentlaan 2
NL - 2280 HV Rijswijk
Tel. (+31-70) 340-2040, Tx. 31 651 epo nl,
Fax: (+31-70) 340-3016

Authorized officer

Plastiras, D

INTERNATIONAL SEARCH REPORT

Int'l Application No

PCT/IT 99/00018

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 4 269 632 A (ROBERTSON KING G ET AL) 26 May 1981 see column 4, line 33 - line 41; figure 1 see column 5, line 14 - line 38 ---	1,6
A	SCHOENBECK J ET AL: "STAND DER ISP-TECHNOLOGIE UND NEUE ENTWICKLUNGEN" STAHL UND EISEN, vol. 116, no. 11, 11 November 1996, pages 65-73, 158, XP000639880 see page 66, right-hand column, line 40 - page 68, right-hand column, line 49 see abstract; figures 6,7,16,19 ---	1,6
A	GOSIO G ET AL: "THE STATUS OF USP AT THE ARVEDI WORKS, CREMONA, ITALY" CAHIERS D'INFORMATIONS TECHNIQUES DE LA REVUE DE METALLURGIE, vol. 93, no. 4, 1 April 1996, pages 551-566, XP000623494 see page 553, left-hand column, line 10 - page 556, left-hand column, line 23 see page 563, right-hand column, line 12 - page 564, line 22 see page 565 ---	1,6
A	DE 38 40 812 A (MANNESMANN AG ;ARVEDI GIOVANNI (IT)) 5 April 1990 cited in the application see figure 1 ---	1,2,6,7
A	EP 0 863 222 A (SCHLOEMANN SIEMAG AG) 9 September 1998 see abstract; figure ---	1,4-6,9, 10
A	DE 195 13 999 A (SUNDWIGER EISEN MASCHINEN) 17 October 1996 see column 2, line 38 - line 42; claims 1,2; figures ---	1,6
A	PATENT ABSTRACTS OF JAPAN vol. 005, no. 206 (M-104), 26 December 1981 -& JP 56 122611 A (KAWASAKI STEEL CORP), 26 September 1981 see abstract; figure -----	5,10

INTERNATIONAL SEARCH REPORT

Information on patent family members

Int. Patent Application No

PCT/IT 99/00018

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
WO 9800248 A	08-01-1998	CA 2225743 A	08-01-1998
		AU 695063 B	06-08-1998
		AU 6360196 A	21-01-1998
		CZ 9704170 A	17-03-1999
		JP 10510587 T	13-10-1998
		PL 327276 A	07-12-1998
		SK 178897 A	09-09-1998
EP 0605947 A	13-07-1994	US 5356495 A	18-10-1994
		AT 167412 T	15-07-1998
		AU 670338 B	11-07-1996
		AU 5199293 A	07-07-1994
		BR 9304938 A	02-08-1994
		CA 2111947 A	29-06-1994
		CN 1093956 A	26-10-1994
		DE 69319217 D	23-07-1998
		DE 69319217 T	21-01-1999
		JP 7011402 A	13-01-1995
		US 5496423 A	05-03-1996
US 4269632 A	26-05-1981	AT 375961 B	25-09-1984
		AT 533679 A	15-01-1983
		AU 523120 B	15-07-1982
		AU 4936079 A	07-02-1980
		CA 1176817 A	30-10-1984
		CH 643001 A	15-05-1984
		DE 2929724 A	14-02-1980
		FR 2412555 A	29-02-1980
		GB 2027744 A, B	27-02-1980
		IN 151384 A	09-04-1983
		NL 7905901 A	06-02-1980
		SE 447129 B	27-10-1986
		SE 7906558 A	05-02-1980
DE 3840812 A	05-04-1990	AT 83409 T	15-01-1993
		AU 624831 B	25-06-1992
		AU 3686289 A	12-12-1989
		BG 51443 A	14-05-1993
		WO 8911363 A	30-11-1989
		DK 171539 B	30-12-1996
		EP 0415987 A	13-03-1991
		FI 92161 B	30-06-1994
		HU 213334 B	28-05-1997
		JP 2726919 B	11-03-1998
		JP 3504572 T	09-10-1991
		KR 9514488 B	02-12-1995
		NO 176085 B	24-10-1994
		RO 108933 A	31-10-1994
		RU 2036030 C	27-05-1995
		US 5307864 A	03-05-1994
		ZW 6589 A	22-11-1989
EP 0863222 A	09-09-1998	DE 19708666 A	10-09-1998
		CN 1197123 A	28-10-1998
		JP 10277603 A	20-10-1998
DE 19513999 A	17-10-1996	NONE	

THIS PAGE BLANK (USPTO)